Dehiscence of patch augmentation of a left-sided atrioventricular valve related to strenuous isometric exercise: Case report and failure analysis

Peter E. Hammer, PhD,a Christopher W. Baird, MD,a Pedro J. del Nido, MD,a and Gerald R. Marx, MD,b Boston, Mass

From the Departments of aCardiac Surgery and bCardiology, Boston Children’s Hospital, Boston, Mass.

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Address for reprints: Peter E. Hammer, PhD, Department of Cardiac Surgery, Boston Children’s Hospital, 300 Longwood Ave, Boston, MA 02115 (E-mail: peter.hammer@childrens.harvard.edu).

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We report a case of the abrupt dehiscence of a patch augmentation of a left-sided atrioventricular valve in a 20-year-old male patient who participated in strenuous isometric exercise. Weight lifting is accompanied by a large blood pressure increase,1 and we hypothesized that the dehiscence was due to elevated loads at the suture line caused by high systolic pressures. To test this hypothesis, we calculated peak estimated load on the valve patch suture line during weight lifting and compared this load with experimental measurements of suture retention in the patch material.

CLINICAL SUMMARY

The 21-year-old male patient had undergone surgery in infancy for primum atrial septal defect and cleft left-sided atrioventricular valve. At 20 years of age, he underwent reoperation for severe regurgitation of the valve, consisting of patch augmentation of the mural leaflet with PhotoFix (CryoLife Inc, Kennesaw, Ga), bovine pericardium stabilized with a dye-mediated photo oxidation fixation process. After surgery, the patient resumed normal activity, including strenuous weight lifting, and he was well until 5 months later, when he experienced sudden onset of dyspnea and exercise intolerance. Echocardiography showed severe regurgitation emanating from the region of the mural leaflet (Figure 1, A). Three-dimensional imaging (Figure 1, B) depicted a disruption in the mural leaflet at the annulus. Intraoperative inspection revealed that the running suture had pulled through the patch at multiple sites along the annulus (Figure 1, C and D, and Video 1).

Analysis of Stress

To analyze the patch dehiscence, we determined the maximum expected leaflet load in a normal mitral valve at typical peak systolic pressures according to published studies.2 During weight lifting, systolic pressures as high as 480 mm Hg have been measured in normotensive subjects.1 Leaflet stress increases in proportion to pressure, so we scaled our estimate to reflect this elevated systolic pressure, yielding an estimate of the maximum expected load on the leaflet near the annulus of 1.6 N/mm. We then measured suture retention strength, which when combined with an estimated suture spacing of 2 mm resulted in a suture line strength of 1.6 N/mm, indicating that the maximum expected load on the repaired valve during weight lifting might indeed reach the level at which the suture line is predicted to fail. See the Appendix for details on the calculation of loads in the valve leaflet and the suture line.

DISCUSSION

For robust design, a structure’s strength should exceed its maximum working load by some safety factor, commonly calculated as the ratio of strength to maximum working load. For our reconstructed valve, we estimate a safety...
factor of \((1.6 \text{ N/mm})/(1.6 \text{ N/mm}) = 1.0\), which corresponds to no margin for safety and is below the range of 2 to 10 commonly seen for both man-made and natural structures.\(^3\) In our experience, acute failure of a valve augmentation patch as seen in the case reported here is rare, suggesting that surgeons are generally quite good at producing repairs of adequate strength. Explicit knowledge of suture retention strength and a true worst-case estimate of transvalvular pressure, however, are necessary to design an adequate repair with confidence. Our results suggest several possibilities for raising the safety factor to ensure against patch dehiscence. Restricting strenuous isometric exercise could lower the peak expected load by one-half or more, increasing the safety factor to at least 2.0. Modifications to the surgical technique could produce a similar effect, however, without requiring exercise restriction. For example, orienting the patch with attention to the material direction could increase the safety factor to 1.7, whereas reducing suture spacing to 1 mm could independently raise it to 2.0. Other factors known to affect suture line strength.
include the size of the suture material, the depth of the suture bite, and incorporation of suture line reinforcement material, although we did not evaluate these factors in this study. We also did not consider the effect of changes to the integrity of the patch with time, nor did we compare suture retention strength in different patch materials, although we think that such a study is necessary. Finally, substantially increasing the size of a leaflet by patch augmentation can result in increased loads at the suture lines. Although it is difficult to precisely predict the magnitude of this effect, it is reasonable to estimate that leaflet stress increases in proportion to the increase in chamber size (Law of Laplace), and we could further scale the estimate for maximum expected load to account for this effect. Despite these limitations, we are hopeful that by adopting a quantitative approach to estimating maximum expected loads and suture line strength, we can avert similar premature failures of surgically repaired valves.

**References**

APPENDIX. SUPPLEMENTARY MATERIAL

Estimation of Loads in the Reconstructed Atrioventricular Valve

Loads within tissue are represented as stress, with units of force per cross-sectional area of tissue. Although stresses in a valve leaflet cannot be measured directly, they can be estimated using computational modeling methods. Leaflet stresses at peak systole are, in general, different in different parts of the valve, and at a given location, leaflet stress can also vary in different directions. For this analysis, we are concerned with stress in the mural leaflet of the left-sided (systemic) atrioventricular valve. Specifically, we are concerned with leaflet stress in the radial direction (Figure 2)—that is, the direction perpendicular to the annulus—because this corresponds to the direction of the loads that resulted in the suture line dehiscence. At normal systolic pressures, peak stress in this region, in the radial direction, is estimated as follows: $400 \text{kPa} = 400,000 \text{N/m}^2 = 0.4 \text{N/mm}^2$. For this analysis, it is more convenient to express leaflet loads as membrane tension, which is the force per length acting on a cross-section of leaflet. Assuming a leaflet thickness of 1 mm, leaflet stress can be converted to membrane tension as follows: $0.4 \text{N/mm}^2 \times 1 \text{mm} = 0.4 \text{N/mm}$. During weight lifting, systolic pressure can increase by a factor of 4.1 Membrane tension is proportional to transvalvular pressure, so, assuming this worst-case scenario for pressure, a 4-fold increase in pressure would produce a 4-fold increase in peak expected membrane tension (Figure 2): $0.4 \text{N/mm} \times 4 = 1.6 \text{N/mm}$.

Estimation of Suture Line Strength

We evaluated suture retention strength with PhotoFix pericardium (CryoLife Inc, Kennesaw, Ga) and 5-0 Prolene suture (Ethicon, Inc, Somerville, NJ), the same materials used in the valve repair. Pericardium is typically characterized by a principal material direction—that is, a direction in the tissue in which elongation under tension is at a minimum. We refer to this as the first principal material direction. In the direction perpendicular, elongation is a maximum, and we refer to this as the second principal material direction. Because this material anisotropy could result in direction-dependent suture retention capacity, we tested suture retention strength in both the first and second principal material directions. In 6 square tissue specimens, 10 mm on a side, a suture was placed 1.0 mm from an edge and tied to form a loop. The loop was placed around the hook of a digital force gauge (model M4; Mark-10 Corporation, Copiague, NY), and the opposite edge of the specimen was secured with a tissue clamp (CellScale Biomaterials Testing, Waterloo, Ontario, Canada), as shown in Figure 3. Tension was applied at a rate of approximately 1 N/s until the suture pulled through the edge of the specimen. Three specimens were tested in each of the 2 principal material directions. Suture pullout force averaged $5.4 \pm 1.0 \text{N}$ and $3.2 \pm 0.2 \text{N}$ in the first and second principal material directions, respectively (Figure 4). The strength of the suture line can be expressed as membrane tension by dividing the suture pullout force by the suture spacing (Figure 5). For the weaker material direction (the second principal material direction) and a suture spacing of 2 mm, the suture line strength is estimated as follows: $(3.2 \text{N/suture})/(2 \text{mm/suture}) = 1.6 \text{N/mm}$.